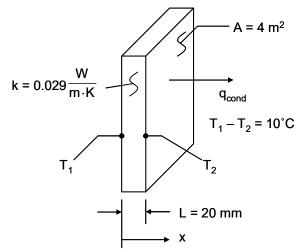
**KNOWN:** Thermal conductivity, thickness and temperature difference across a sheet of rigid extruded insulation.

**FIND:** (a) The heat flux through a  $2 \text{ m} \times 2 \text{ m}$  sheet of the insulation, and (b) The heat rate through the sheet.

**SCHEMATIC:** 



**ASSUMPTIONS:** (1) One-dimensional conduction in the x-direction, (2) Steady-state conditions, (3) Constant properties.

ANALYSIS: From Equation 1.2 the heat flux is

$$q_x'' = -k\frac{dT}{dx} = k\frac{T_1 - T_2}{L}$$

Solving,

$$q''_{x} = 0.029 \frac{W}{m \cdot K} \times \frac{10 \text{ K}}{0.02 \text{ m}}$$

$$q''_{x} = 14.5 \frac{W}{m^{2}}$$
(4)

The heat rate is

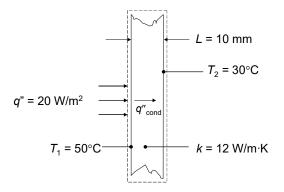
$$q_x = q''_x \cdot A = 14.5 \frac{W}{m^2} \times 4 m^2 = 58 W$$
 <

**COMMENTS:** (1) Be sure to keep in mind the important distinction between the heat flux  $(W/m^2)$  and the heat rate (W). (2) The direction of heat flow is from hot to cold. (3) Note that a temperature *difference* may be expressed in kelvins or degrees Celsius.

**KNOWN:** Thickness and thermal conductivity of a wall. Heat flux applied to one face and temperatures of both surfaces.

FIND: Whether steady-state conditions exist.

**SCHEMATIC**:



**ASSUMPTIONS**: (1) One-dimensional conduction, (2) Constant properties, (3) No internal energy generation.

ANALYSIS: Under steady-state conditions an energy balance on the control volume shown is

$$q_{in}'' = q_{out}'' = q_{cond}'' = k(T_1 - T_2)/L = 12 \text{ W/m} \cdot \text{K}(50^{\circ}\text{C} - 30^{\circ}\text{C})/0.01 \text{ m} = 24,000 \text{ W/m}^2$$

<

Since the heat flux in at the left face is only 20  $W/m^2$ , the conditions are not steady state.

**COMMENTS:** If the same heat flux is maintained until steady-state conditions are reached, the steady-state temperature difference across the wall will be

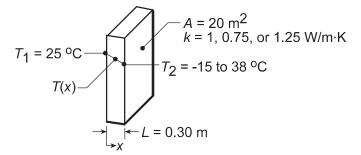
$$\Delta T = q''L/k = 20 \text{ W/m}^2 \times 0.01 \text{ m}/12 \text{ W/m} \cdot \text{K} = 0.0167 \text{ K}$$

which is much smaller than the specified temperature difference of 20°C.

KNOWN: Inner surface temperature and thermal conductivity of a concrete wall.

**FIND:** Heat loss by conduction through the wall as a function of outer surface temperatures ranging from -15 to 38°C.

### **SCHEMATIC:**



**ASSUMPTIONS:** (1) One-dimensional conduction in the x-direction, (2) Steady-state conditions, (3) Constant properties.

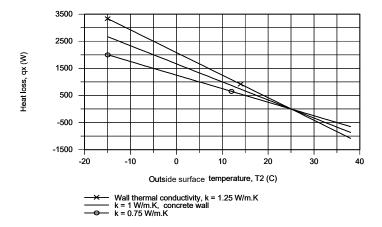
**ANALYSIS:** From Fourier's law, if  $q''_X$  and k are each constant it is evident that the gradient,

 $dT/dx = -q''_X/k$ , is a constant, and hence the temperature distribution is linear. The heat flux must be constant under one-dimensional, steady-state conditions; and k is approximately constant if it depends only weakly on temperature. The heat flux and heat rate when the outside wall temperature is  $T_2 = -15^{\circ}C$  are

$$q''_{x} = -k\frac{dT}{dx} = k\frac{T_{1} - T_{2}}{L} = 1 W/m \cdot K \frac{25^{\circ}C - (-15^{\circ}C)}{0.30 m} = 133.3 W/m^{2}.$$
 (1)

$$q_{\rm X} = q_{\rm X}'' \times A = 133.3 \,{\rm W}/{\rm m}^2 \times 20 \,{\rm m}^2 = 2667 \,{\rm W} \,.$$
 (2) <

Combining Eqs. (1) and (2), the heat rate  $q_x$  can be determined for the range of outer surface temperature,  $-15 \le T_2 \le 38^{\circ}$ C, with different wall thermal conductivities, k.



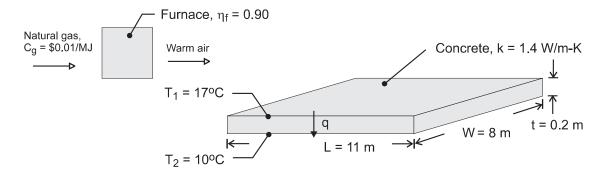
For the concrete wall, k = 1 W/m·K, the heat loss varies linearly from +2667 W to -867 W and is zero when the inside and outer surface temperatures are the same. The magnitude of the heat rate increases with increasing thermal conductivity.

**COMMENTS:** Without steady-state conditions and constant k, the temperature distribution in a plane wall would not be linear.

**KNOWN:** Dimensions, thermal conductivity and surface temperatures of a concrete slab. Efficiency of gas furnace and cost of natural gas.

FIND: Daily cost of heat loss.

## **SCHEMATIC:**



**ASSUMPTIONS:** (1) Steady state, (2) One-dimensional conduction, (3) Constant properties. **ANALYSIS:** The rate of heat loss by conduction through the slab is

$$q = k (LW) \frac{T_1 - T_2}{t} = 1.4 W / m \cdot K (11m \times 8m) \frac{7^{\circ}C}{0.20m} = 4312 W$$

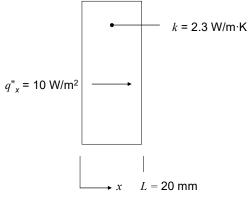
The daily cost of natural gas that must be combusted to compensate for the heat loss is

$$C_{d} = \frac{qC_{g}}{\eta_{f}} (\Delta t) = \frac{4312 \,W \times \$0.02 \,/\,MJ}{0.9 \times 10^{6} \,J \,/\,MJ} (24 \,h \,/\,d \times 3600 \,s \,/\,h) = \$8.28 \,/\,d$$

**COMMENTS:** The loss could be reduced by installing a floor covering with a layer of insulation between it and the concrete.

**KNOWN:** Thermal conductivity and thickness of a wall. Heat flux through wall. Steady-state conditions.

**FIND:** Value of temperature gradient in K/m and in °C/m. **SCHEMATIC**:



ASSUMPTIONS: (1) One-dimensional conduction, (2) Constant properties.

ANALYSIS: Under steady-state conditions,

$$\frac{dT}{dx} = -\frac{q_x^{"}}{k} = -\frac{10 \text{ W/m}^2}{2.3 \text{ W/m} \cdot \text{K}} = -4.35 \text{ K/m} = -4.35 \text{ °C/m}$$

Since the K units here represent a temperature *difference*, and since the temperature difference is the same in K and °C units, the temperature gradient value is the same in either units.

**COMMENTS:** A negative value of temperature gradient means that temperature is decreasing with increasing *x*, corresponding to a positive heat flux in the *x*-direction.